# Drying of cohesive particles in vibrated fluidized beds

## Modeling hydrodynamics under mechanical vibration

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#### **Motivation**





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#### Cohesive powders gain importance:

nano-particles, pharmaceutical and food powders

#### Vibration enhances fluidization of cohesive powders:

- vibrated fluidized bed (VFB) research only in lab-scale
- scarce research on VFB drying of milk powder











\* Lehmann et al., Fluidization characteristics of cohesive powders in vibrated fluidized bed drying at low vibration frequencies, Powder Technology, accepted

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#### Methods Modeling approach



Basis: Alaathar [1,2]

- steady state model of continuous fluidized bed dryers
- for Geldart B particles
- distributed parameters: T,  $d_p$ , x,  $\tau$
- drying kinetics model [3 5]
- fluid mechanics model [6]
- key parameter: bubble volume fraction  $\varepsilon_b$

#### **Required adjustments:**

- dynamic model
- cohesive powders
- influence of vibration
- [1] Alaathar et al., Powder Technology 238, (2013) [2] Alaathar, PhD Thesis, TUHH, (2017)
- [3] Groenewold and Tsotsas, Drying Technology, 15 (1997)
- [4] Burgschweiger et al., Can. Journ. of Chem. Engin., 77 (1999)
- [5] Burgschweiger and Tsotsas, Chem. Engin. Science, 57 (2002)
- [6] Werther and Wein, AIChE Symp., 90 (1994)



#### Methods Experiments



#### Material:

Whole milk powder					
$ ho_s$	[kg/m³]	866.4±73.5			
$d_{32}$	[µm]	101.7±1.3			

## Investigated process parameters:

- gas flow rate
- vibration intensity  $\Lambda$

$$\Lambda = \frac{a_{vibration}}{g} = \frac{(2\pi f)^2 \cdot A_{vib}}{g}$$



Whole milk powder: x = 4 wt.-%; m = 12.5 kg; u = 0.3 m/s;  $\Lambda = 0.58$ 

#### Analysis of fluid mechanics via:

- Δp measurement
- visual observation (high speed camera)

#### **Characteristics:**

- bed expansion
- gas hold-up / bubble volume fraction
- lower limit of fluidization (u<sub>mf</sub>)

 $\rho_s$ : particle density;  $d_{32}$ : Sauter mean diameter; *X*: powder moisture content; *f*: frequency;  $A_{vib}$ : amplitude, *g*: gravitational acceleration;  $\Lambda$ : vibration intensity

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frequency	f	[Hz]	0	4	6	8	10	
amplitude	A <sub>vib</sub>	[mm]	0	5	4	3.5	3	
intensity	Λ	[-]	0	0.32	0.58	0.90	1.21	

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Minimum fluidization velocity u<sub>mf</sub>:



Whole milk powder: x = 4 wt.% m = 25 kg



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#### Bed expansion:

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 $\varepsilon = 1 - \frac{m}{A \cdot h \cdot \rho_s}$ 





Whole milk powder: x = 4 wt.%, m = 12.5 kg;  $\varepsilon_{\text{bulk}} = 0.53$ 

 $h_{vib}$ 

0.25





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#### Image analysis:

- high speed image series (100 fps)
- segmentation of grey scale image series (Matlab)
- calculate bubble volume fraction (Matlab)

- non-invasive
- global measurement
- only at the glass wall (2D plane)

vibrated fluidized

Valid representation of hydrodynamics inside the bed for low excess gas velocities (u-u<sub>mf</sub> < 0.25) [7]



[7] Lehmann et al., Fluidization characteristics of cohesive powders in vibrated fluidized bed drying at low vibration frequencies, Powder Technology, accepted

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- slight decrease of bubble volume fraction
- increase of bed expansion
- vibration causes expansion of suspension phase
- explains increased heat and mass transfer rates

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#### **Results** Modeling



#### **Bubble volume fraction:**

• modified correlation from Hilligardt and Werther [8]

$$\varepsilon_{b} = \frac{\dot{V}_{b}}{u_{b}}$$
$$u_{b} = \dot{V}_{b} + 0.71 \cdot \vartheta \cdot \sqrt{g \cdot d_{v}}$$
$$\dot{V}_{b} = \Psi \cdot \left(u - u_{mf}\right) \cdot \frac{1}{(1 + \Lambda)}$$

#### **Bubble diameter:**

- correlation from Zou et al. [9]
- for cohesive particles

$$d_{v} = 0.21 \cdot \frac{\left(u - u_{mf}\right)^{0.49} \cdot \left(h + 4\sqrt{A_{0}}\right)^{0.48}}{a^{0.2}}$$

[8] Hilligardt and Werther, Ger. Chem. Eng. 9 (1986), 215-221 [9] Zou et al., Powder Technology 212 (2011), 258-266

Whole milk powder: x = 4 wt.-%, m = 25 kg, u = 0.2 m/s



#### **bold**: vibration dependent parameter

 $d_{v}$ : bubble diameter; *h*: height over distributor;  $\varepsilon_{b}$ : local bubble volume fraction;  $u_{b}$ : bubble rise velocity; *g*: gravitational acceleration;  $\vartheta$ : hydrodynamic constant; *u*: gas velocity;  $u_{mf}$ : minimum fluidization velocity;  $\dot{V}_{b}$ : apparent gas flow rate per bubble cross sectional area;  $\Psi$ : hydrodynamic parameter for bed dimensions;  $A_{0}$ : cross sectional area of distributor orifices ( $A_{0} \approx 0$  for porous plate)

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#### Results Modeling

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#### **Bed porosity:**

 $\varepsilon = 1 - (1 - \varepsilon_b)(1 - \varepsilon_d)$ 

Porosity of dense phase:

 modified Richardson and Zaki correlation [10]

$$\varepsilon_d = \varepsilon_{mf} \cdot \left(\frac{u_d}{u_{mf}}\right)^{\frac{1}{4.65 \cdot (1+\Lambda)}}$$

Gas velocity in dense phase:

• according to Clift et al. [11]

 $u_d = \boldsymbol{u_{mf}} \cdot (1 + 1.5 \cdot \boldsymbol{\varepsilon_b})^{\frac{2}{3}}$ 

[10] Richardson and Zaki, Chem. Eng. Sci., 3 (1954), 65-73[11] Clift et al., Fluidization 4 - Proceedings, (1983), 77-85

 $\varepsilon$ : bed porosity;  $\varepsilon_d$ : porosity of dense phase;  $\varepsilon_b$ : local bubble volume fraction;  $\varepsilon_{mf}$ : bed porosity at minimum fluidization;  $u_d$ : gas velocity in dense phase;  $\Lambda$ : vibration intensity;  $u_{mf}$ : minimum fluidization velocity



**bold**: vibration dependent parameter

#### Set of modified correlations:

> good prediction of  $\varepsilon_b$  and  $\varepsilon$  under vibration

#### Conclusion

#### Summary:

Pilot plant scale VFB dryer for comprehensive experiments:

Effect of vibration:

- reduces u<sub>mf</sub>
- reduces bubble volume fraction
- increases bed expansion
- expansion of suspension phase

Modeling of hydrodynamics under vibration:

- set of modified correlations for prediction of
  - bubble volume fraction
  - bed porosity
- correlation are unchanged for non-vibrated cases





#### **Outlook:**

- testing model for other cohesive powders
- dynamic modeling of VFB dryers

### Thank you for your attention!

