### Progress on Moisture Swing Sorbents

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April 2014

# **Three Rules for Technological Fixes**

#### **D. Sarewitz and Richard Nelson:**

Three rules for technological fixes, *Nature*, 2008, 456, 871-872

- I. The technology must largely embody the cause-effect relationship connecting problem to solution.
- II. The effects of the technological fix must be assessable using relatively unambiguous or uncontroversial criteria.
- III. Research and development is most likely to contribute decisively to solving a social problem when it focuses on improving a standardized technical core that already exists.

"... direct removal of  $CO_2$  from the atmosphere — air capture — satisfies the rules for technological fixes. Most importantly, air capture embodies the essential cause–effect relations — the basic go — of the climate change problem, by acting directly to reduce  $CO_2$  concentrations, independent of the complexities of the global energy system (Rule I). There is a criterion of effectiveness that can be directly and unambiguously assessed: the amount of  $CO_2$  removed (Rule II). And although air-capture technologies have been remarkably neglected in both R&D and policy discussions, they nevertheless seem technically feasible (Rule III)."

# Make the air do your work



#### • Air carries kinetic energy

• Plenty to move the air

#### $\circ$ Air carries thermal energy

• sufficient to evaporate water

#### • Air carries chemical potential

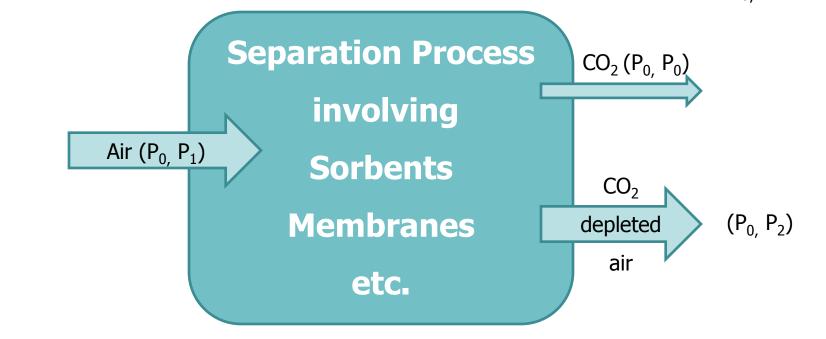
- out of equilibrium with water
- sufficient to compress CO<sub>2</sub> two hundredfold

#### Take advantage of the resource you have

# Separation of a gas stream

Theoretical minimum free energy requirement for the regeneration is the free energy of mixing

Gas pressure  $P_0$ CO<sub>2</sub> partial pressure  $P_x$ Denoted as ( $P_0$ ,  $P_x$ )

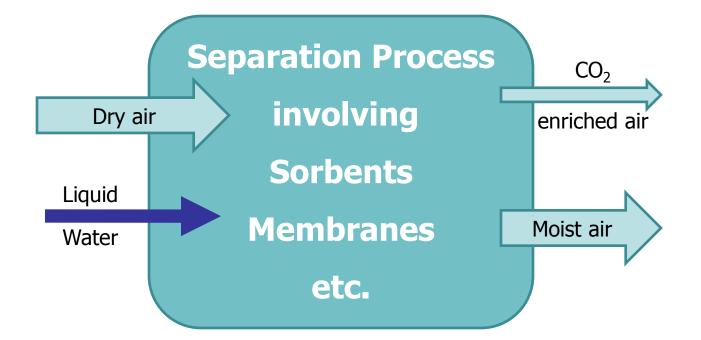


$$\Delta G = RT \left( \left( \frac{P_0 - P_2}{P_1 - P_2} \right) \frac{P_1}{P_0} \ln \frac{P_1}{P_0} - \left( \frac{P_0 - P_1}{P_1 - P_2} \right) \frac{P_2}{P_0} \ln \frac{P_2}{P_0} + \left( \frac{P_0 - P_1}{P_0} \right) \left( \frac{P_0 - P_2}{P_0} \right) \frac{P_0}{P_1 - P_2} \ln \frac{P_0 - P_1}{P_0 - P_2} \right) \frac{P_0}{P_0 - P_2} \ln \frac$$

Specific irreversible processes have higher free energy demands

# Free energy from water evaporation

Water evaporation can drive CO<sub>2</sub> capture

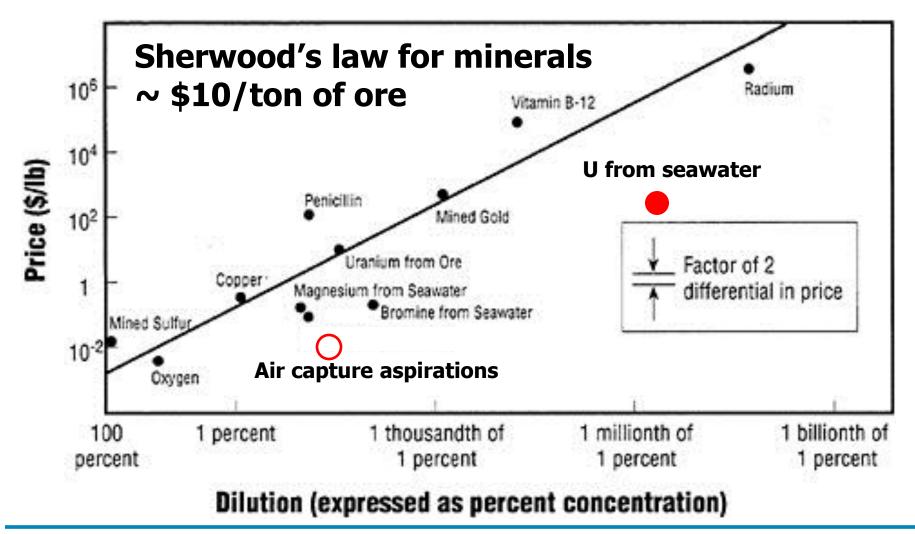


Free energy of water evaporation at a relative humidity *RH:*  $\Delta G = RT \ln(P/P_{sat}) = RT \ln(RH)$ 

Ball park estimate: 2.5 kJ/mol 140 MJ/m<sup>3</sup> @ 20¢/m<sup>3</sup> 0.5¢/kWh

### **Capture of CO<sub>2</sub> from ambient air**

#### not your run-of-the-mill separation problem



#### Artificial kelp to absorb uranium from seawater

#### • Passive, long term exposure to water

- Braids of sorbent covered buoyant plastic
- Anchored to the floor
- Replaced initially active systems

#### Low energy sorbent

- Laminar flow over sorbent
- Uptake is limited by boundary layer transport

#### Regeneration

 $\circ~$  After harvesting the strings

#### • Gross violation of Sherwood's Law

- Cost estimates range from \$200 to \$1200/kg
- Sherwood \$3 million/kg



#### Artificial kelp to absorb uranium from seawater

- Passive, long term exposure to water
  - Braids of sorbent covered buoyant plastic
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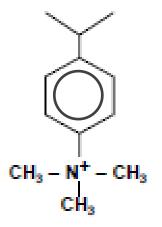
# Coster = offent b + c log(D) • Laminar flow over sorbent

- Uptake is limited by boundary layer transport
- Regeneration
  - After harvesting the strings must make a small
- Gross violation of Sherwood's Lav
  - Cost estimates range from \$200 to \$1200/kg
  - Sherwood \$3 million/kg

### **Anionic Exchange Resins**

#### Solid carbonate "solution" Quaternary ammonium ions form strong-base resin

Type I Strong Base Resins



- Positive ions fixed to polymer matrix

   Negative ions are free to move
   Negative ions are hydroxides, OH<sup>-</sup>
- Dry resin loads up to bicarbonate  $\circ OH^- + CO_2 \rightarrow HCO_3^-$  (hydroxide  $\rightarrow$  bicarbonate)
- Wet resin releases  $CO_2$  to carbonate  $\circ$  2HCO<sub>3</sub><sup>-</sup>  $\rightarrow$  CO<sub>3</sub><sup>--</sup> + CO<sub>2</sub> + H<sub>2</sub>O

#### **Moisture driven CO<sub>2</sub> swing**

# **Membrane material**

# thin sheets

Snowpure electrochemical membrane (1mm thick)

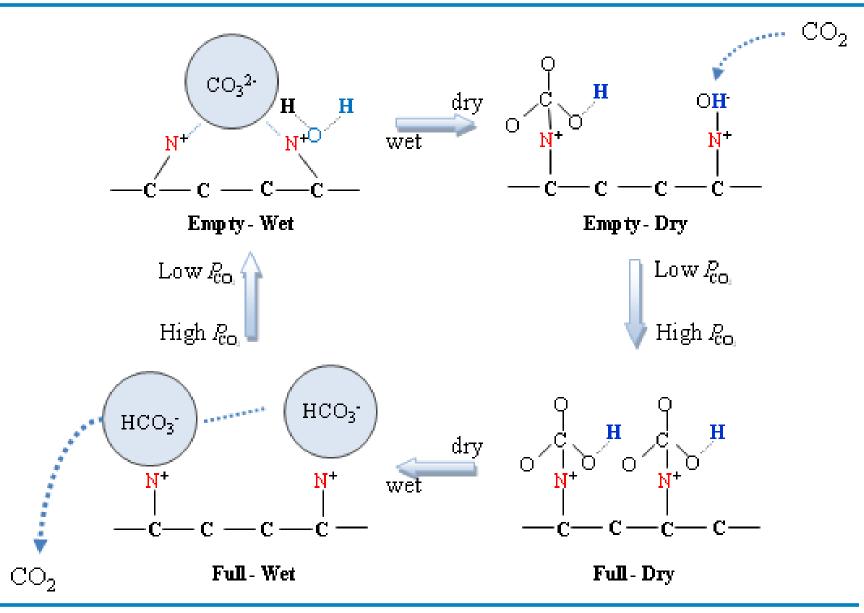
Polypropylene matrix with embedded fine resin particles (25µm)

Quaternary ammonium cations Carbonate/bicarbonate form

1.7 mol/kg charge equivalent



### The moisture swing – water driven



### **Progress on several fronts**

### Better form factors

• Embedded resin powder into paper matrix

### Protection from liquids

Tyvek and similar barriers

### Alternative Sorbents

Activated carbon impregnated with carbonate

### • Molecular dynamics results

• Humidity swing is calculable

# Paper Air Filters

# A Tyvek<sup>®</sup> Pouch



# **Alternative sorbent options**

#### Activated carbon

 $\circ$  No discernable moisture swing

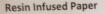
#### Carbonate brines

No discernable moisture swing

#### Carbon impregnated with carbonate

- $\circ$  Strong moisture swing
- Moisture induced pressure change is small

# **Different materials for sorption**



Potassium Carbonate

Sodium Carbonate

Norit<sup>®</sup> RBAA 1 Carbon

Norit® RBAA 1 + Sodium Carbonate

Norit<sup>®</sup> Darco G60

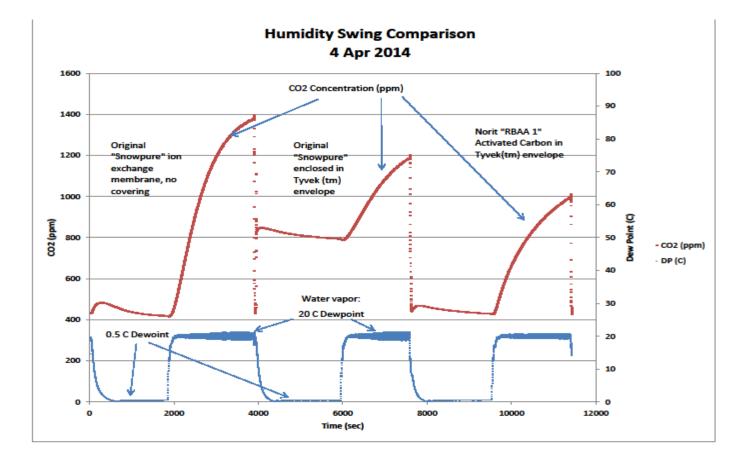
Norit® Darco G60 + Sodium Carbonate



### Different samples tested for moisture swing

### **Tyvek® barrier for sample comparison**

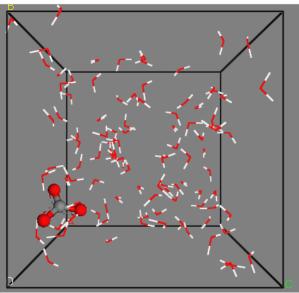
Membrane without Tyvek<sup>®</sup>, with Tyvek<sup>®</sup>, and Carbonate impregnated activated carbon



# **Molecular dynamics calculations**

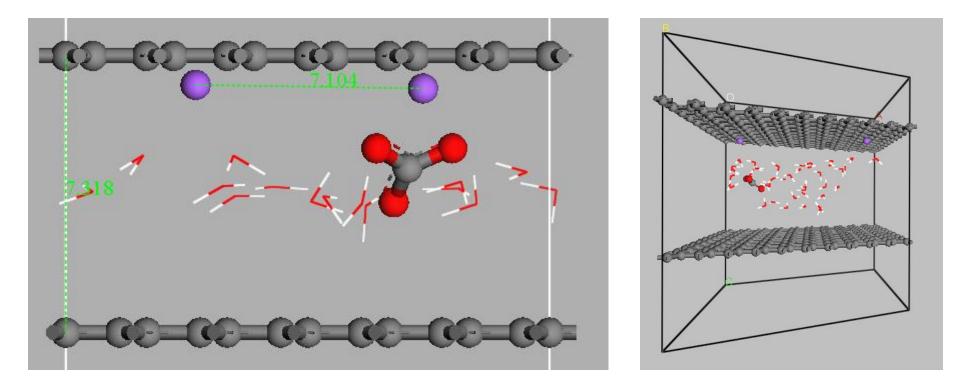
#### **Xiaoyang Shi**

- Learned how to set up models
- Learned how to run test examples
- Using mainly public domain software
   Affordability
  - $\circ$  Flexibility



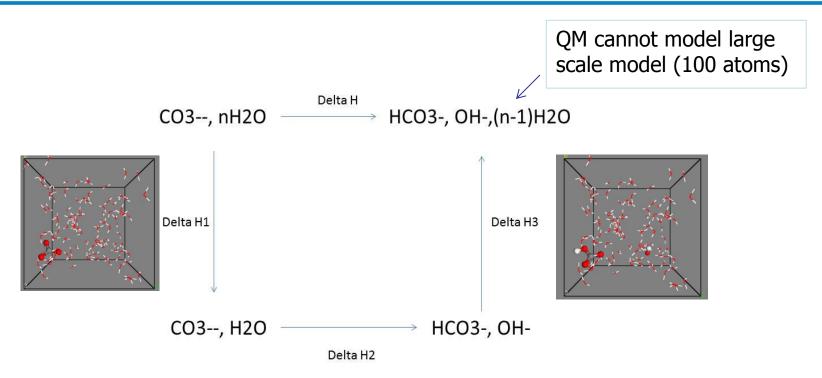
Carbonate ion hydration

# **Geometry Configurations of Models**



Purple atoms are fixed cations (fashioned after sodium), grey atoms are graphene as confined layers, and carbonate ions with water molecules are in the confined region.

# Methodology



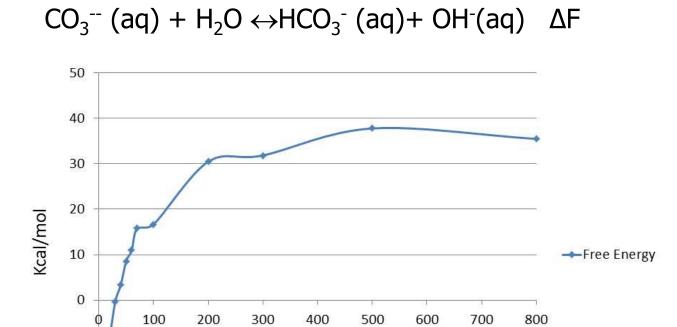
Delta H= Delta H1 + Delta H2 + Delta H3

 $CO_3^{--} \cdot nH_2O \Leftrightarrow HCO_3^{-} \cdot m_1H_2O + OH^{-} \cdot m_2H_2O + (n-1-m_1-m_2)H_2O$ 

 $CO_3^{--} + H_2O \Leftrightarrow HCO_3^{-} + OH^{-}$ 

reaction energy is -48.3255 kcal/mol based on QM calculation

# Free Energy Change with Humidity



Number of water molecules

-10

-20

-30

Carbonate ion and bicarbonate with hydroxide ions free energy changes with the number of water molecules in the calculational volume